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# MHD PERISTALTIC FLOW OF A COUPLE STRESS FLUIDS PERMEATED WITH SUSPENDED PARTICLES THROUGH A POROUS MEDIUM UNDER LONG WAVELENGTH APPROXIMATION

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#### ABSTRACT

The MHD peristaltic flow of a couple stress fluid permeated with suspended particles through a porous medium in two dimensional flexible channel under long wave length and low Reynolds approximation is studied. An analytical method of solution is obtained in terms of wall slope parameter and closed form of expressions has been derived for axial velocity and transverse velocity in fluid phase and particle phase. The expression for velocity profile and pressure gradient and the volumetric flow rate in the wave frame is obtained. The graphical results obtained for velocity profile and pressure gradient. It is observe that velocity profile decreases with increase in Hartmann number M and couple stress parameter S. The pressure gradient has an opposite behavior compared with velocity profile for Hartmann number M.

Keywords: peristaltic flow, couple stress fluid, MHD, suspended particles, velocity profile, pressure gradient, porous.

#### 1. INTRODUCTION

The movement of body fluids travelling through tubular organs continuously by contraction and relaxation due to change in pressure along the walls is called Peristaltic movement takes place while peristalsis. swallowing food through the oesophagus to the stomach, transport of lymph on lymphatic vessels, vasomotion of small blood vessels tube, capillaries vennules and arteries, transport of chyme through the small intestine, the feces movement in the large intestine, the passage of urine from the kidneys through the ureter to the urinary bladder, the flow of semen in the male reproductive tract, and the movement of ovum in the female fallopian tube. Peristaltic phenomenon is used in biomedical instruments like dialysis machines, heart lung machines, artificial heart and ortho machines and transport of toxic material waste inside the sanitary ducts, peristaltic concept is used in nuclear industry to avoid contamination of the outside environment.

For the recent contribution, we refer the reader to [1-20] and the references cited therein. The study of peristaltic transport in experimental and analytical situations has recently become the object of scientific research, since the first investigation by T. W. Latham [3]. J. C. Burns and Parkes [2] has first considered the low Reynolds number in his article of peristaltic motion. A very important investigation is made by Shapiro and Jaffrin [6]. He only initiated the concept of long wavelength and low Reynolds number approximation. Brown and Hung [1] had set the Reynolds number as finite. Moreover they discussed two dimensional peristaltic flow in both computational and experimental situations in detail. Vazravelu, Radharishnamacharya and Radhakrishna-murthy [16] discussed peristaltic flow and heat transfer in a vertical porous annulus with long wave approximation. Rathod and Asha [18] studied the effect of magnetic field and an endoscope on Peristaltic motion in uniform and non-uniform annulus under low Reynolds number approximation.

The theory of couple stress was first developed by Stokes [14] and represents the simple generalization of classical theory which allows for polar effects such as presence of couple stress and body couples. A few examples of such fluids consisting of rigid, randomly oriented particles (red cells), suspended in a viscous medium, such as blood, lubricants containing small amount of polymer additive, electro-rheological fluids and synthetic fluids. Several authors Valanis and Sun, Chaturani, Chaturani and Rathod, Srivastava, Mekheimer, Sobh, Raghunatha Rao and Prasada Rao have studied couple stresses in peristaltic flow [15, 8, 9, 13, 4, 12, 10]. The study of two-phase flows finds applications in many branches of Engineering, Environmental, Physical Sciences, etc. A few examples of such flows in diverse fields are the flow of dissolved micro molecules of fiber suspensions in paper making, flow of blood through arteries, propulsion and combustion in rockets, dispersion and fall out of pollutants in air, erosion of material due to continuous impingement of suspended particles in air etc. It dusty fluid serves as a better model to describe blood as a binary system. Solid-particle motion in two-dimensional peristaltic flows has been discussed by Hung and Brown [1]. Dust velocity shear driven rotational waves and associated vertices in a non-uniform dusty plasma has been investigated by Subba Reddy, Jayarami Reddy, Nagendra and Swaroopa [19], Rami Reddy and Venkataramana [20] studied unsteady flow of a dusty fluid between two oscillating plates under varying constant pressure gradient, Ravi kumar and sivaprasad [17] discussed the peristaltic flow of a dusty couple stress fluid in a flexible channel. T. Raghunath Rao and D. R. V. Prasada Rao [7] discussed the peristaltic transport of a couple stress fluid permeated with suspended particles. Ravikumar [11] studied peristaltic flow of a dusty couple



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stress fluid in a flexible channel. Mekheimer, Husseny and Elmaboud [5] studied the effects of heat transfer and space porosity on peristaltic flow in a vertical asymmetric channel.

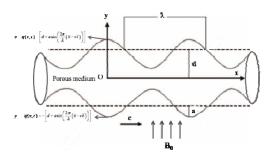
In this present article MHD peristaltic flow of a couple stress fluid permeated with suspended particles through a two dimensional flexible channel under long wave length and low Reynolds approximation is studied. A analytical method of solution is obtained in terms of wall slope parameter and closed form of expressions has been derived for axial velocity and transverse velocity in fluid phase and particle phase. The expression for velocity profile and pressure gradient and the volumetric flow rate in the wave frame is obtained. The graphical results are obtained for velocity profile and pressure gradient for various parameter.

# 2. FORMULATION OF THE PROBLEM

We consider a peristaltic flow of a couple stressdusty fluids through two-dimensional channel bounded by flexible walls. The geometry of the flexible walls are represented by

$$y = \eta(X, t) = d + a \sin \frac{2\pi}{\lambda} (X - ct)$$
 (1)

Where 'd' is the mean half width of the channel, 'a' is the amplitude of the peristaltic wave, 'c' is the wave velocity.  $\lambda$  is the wave length and t is the time.



**Figure-1.** Physical representation of 2-Dimensional flexible channel.

The equations governing the two-dimensional flow of a couple stress fluid permeated with suspended particles in fluid phase and particle phase are

$$\begin{split} &\frac{\partial \overline{u}}{\partial \overline{x}} + \frac{\partial \overline{v}}{\partial \overline{y}} = 0 \\ &\rho \left( \frac{\partial \overline{u}}{\partial \overline{t}} + \overline{u} \frac{\partial \overline{u}}{\partial \overline{x}} + \overline{v} \frac{\partial \overline{u}}{\partial \overline{y}} \right) = -\frac{\partial \overline{p}}{\partial \overline{x}} + \mu \nabla^2 \overline{u} + \eta^* \nabla^4 \overline{u} \\ &+ KN(\overline{u}_p - \overline{u}) - \sigma B_0^2 \overline{u} - \frac{\mu}{k_0} \overline{u} \end{split} \tag{2}$$

$$\rho \left( \frac{\partial \overline{v}}{\partial \overline{t}} + \overline{u} \frac{\partial \overline{v}}{\partial \overline{x}} + \overline{v} \frac{\partial \overline{v}}{\partial \overline{y}} \right) = -\frac{\partial \overline{p}}{\partial \overline{y}} + \mu \nabla^2 \overline{v} + \eta^* \nabla^4 \overline{v}$$

$$+ KN(\overline{v}_p - \overline{v}) - \frac{\mu}{k_0} \overline{v}$$

$$(4)$$

For dust particles

$$\frac{\partial N}{\partial \overline{x}} + N \left( \frac{\partial \overline{u}_p}{\partial \overline{x}} + \frac{\partial \overline{v}_p}{\partial \overline{y}} \right) = 0$$
 (5)

$$\left(\frac{\partial \overline{u}_p}{\partial \overline{t}} + \overline{u}_p \frac{\partial \overline{u}_p}{\partial \overline{x}} + \overline{v}_p \frac{\partial \overline{u}_p}{\partial \overline{y}}\right) = \frac{k}{m} (\overline{u} - \overline{u}_p)$$
(6)

$$\left(\frac{\partial \overline{v}_p}{\partial \overline{t}} + \overline{u}_p \frac{\partial \overline{v}_p}{\partial \overline{x}} + \overline{v}_p \frac{\partial \overline{v}_p}{\partial \overline{y}}\right) = \frac{k}{m} (\overline{v} - \overline{v}_p)$$
(7)

$$\nabla^2 = \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}\right), \nabla^4 = \nabla^2 \nabla^2$$
(8)

where  $\overline{u}, \overline{v}$  is the velocity of the fluid particles,  $\overline{u}_p, \overline{v}_p$  is the velocity of the dust particles,  $\overline{p}$  is the fluid pressure,  $\sigma$  is the electrical conductivity of the fluid,  $B_0$  is the applied magnetic field,  $\rho$  is the density of the fluid, v is the kinematic coefficient of the viscosity of fluid, and  $K=6\pi\mu r$ , r being the particle radius, is the Stoke's drag coefficient for the dust particles(a constant), m is the mass of the solid particles, m is the coefficient of couple stress, n is the number density of the particle, n is the coefficient of viscosity, n is the stokes resistance coefficient, n is the permeability of the porous medium. The corresponding boundary conditions are

$$\overline{u} = 0$$
 at  $\overline{y} = \pm \eta$ 

$$\frac{\partial^2 \overline{u}}{\partial \overline{y}^2} = 0$$
 at  $\overline{y} = \pm \eta$ 

$$\overline{v} = 0$$
 at  $\overline{y} = 0$  (9)

Introducing a wave frame (x,y) moving with velocity c awayfrom the fixed frame (X,Y) by the transformation

$$\overline{x} = X - c\overline{t}, \overline{y} = Y, \overline{u} = U - c, \overline{v} = V, \overline{p} = P(X, t)$$

Introducing the following non dimensional quantities

$$x = \frac{\overline{x}}{\lambda}, y = \frac{\overline{y}}{d}, u = \frac{\overline{u}}{c}, u_p = \frac{\overline{u}_p}{c}, v = \frac{\overline{v}}{c}, v_p = \frac{\overline{v}_p}{c}, \eta = \frac{\overline{\eta}}{d}, t = \frac{v\overline{t}}{\lambda}$$

Equations (1) to (9) reduced as

$$y = \eta(x) = 1 + \varepsilon \sin 2\pi x \tag{10}$$

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(12)

$$R\delta\left(\frac{\partial u}{\partial t} + u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}\right) = -\frac{\partial p}{\partial x} + \left(\delta^{2}\frac{\partial^{2} u}{\partial x^{2}} + \frac{\partial^{2} u}{\partial y^{2}}\right) + S\left(\delta^{2}\frac{\partial^{2} u}{\partial x^{2}} + \frac{\partial^{2} u}{\partial y^{2}}\right)\left(\delta^{2}\frac{\partial^{2} u}{\partial x^{2}} + \frac{\partial^{2} u}{\partial y^{2}}\right) + \frac{R\alpha}{\tau}(u_{p} - u) - \left(M^{2} + \frac{1}{k_{1}}\right)u$$
(11)

$$R\delta^{3} \left( \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} \right) = -\frac{\partial p}{\partial y} + \delta^{2} \left( \delta^{2} \frac{\partial^{2} v}{\partial x^{2}} + \frac{\partial^{2} v}{\partial y^{2}} \right) +$$

$$\pi \delta^{3} \left( \delta^{2} \frac{\partial^{2} v}{\partial x} + v \frac{\partial^{2} v}{\partial y} \right) \left( \delta^{2} \frac{\partial^{2} v}{\partial y} + \delta^{2} v \right)$$

$$S\delta^{2} \left( \delta^{2} \frac{\partial^{2}}{\partial x^{2}} + \frac{\partial^{2}}{\partial y^{2}} \right) \left( \delta^{2} \frac{\partial^{2} v}{\partial x^{2}} + \frac{\partial^{2} v}{\partial y^{2}} \right) + \frac{R\alpha}{2} \delta^{2} (v_{p} - v) + \delta^{2} \frac{1}{V} v$$

For dust particles

$$\delta \left( \frac{\partial u_p}{\partial t} + u_p \frac{\partial u_p}{\partial x} + v_p \frac{\partial u_p}{\partial y} \right) = \frac{1}{\tau} (u - u_p)$$
(13)

$$\delta \left( \frac{\partial v_p}{\partial t} + v_p \frac{\partial v_p}{\partial x} + v_p \frac{\partial v_p}{\partial y} \right) = \frac{1}{\tau} (v - v_p)$$
(14)

Where  $\varepsilon = \frac{a}{d}$  and  $\delta = \frac{d}{\lambda}$  are geometric

parameters, 
$$R = \frac{cd}{v}$$
 is the Reynolds number,  $S = \frac{\eta^*}{\mu d^2}$  is

$$\alpha = \frac{1}{\rho}$$
 is t

 $\alpha = \frac{Nm}{\rho}$  the couple stress parameter,  $\alpha = \frac{Nm}{\rho}$  is the dust

concentration parameter,  $\tau = \frac{cm}{kd}$  is the relaxation time,

$$M^2 = B_0 d \sqrt{\frac{\sigma}{\mu}}$$
 is the Hartmann number,  $k_0 = \frac{K_1}{d^2}$  is the coefficient of permeability of porous medium,

The corresponding non dimensional boundary conditions

$$u = -1 at y = \pm \eta$$

$$\frac{\partial^2 u}{\partial y^2} = 0 at y = \pm \eta$$

$$v = 0 at y = 0$$
(15)

# SOLUTION OF THE PROBLEM

Using approximation of the long wavelength  $(i.e \delta \Box 1)$ and neglecting the wave number and with approximation of the low Reynolds number  $(i.e \, \text{Re} \rightarrow 0)$ , we get

$$S\frac{\partial^4 u}{\partial y^4} - \frac{\partial^2 u}{\partial y^2} - \frac{R\alpha}{\tau}(u_p - u) + L^2 u = -\frac{\partial p}{\partial x}$$
(16)

$$0 = -\frac{\partial p}{\partial y} \tag{17}$$

$$0 = \frac{1}{\tau} (u - u_p) \tag{18}$$

$$0 = \frac{1}{\tau} (v - v_p) \tag{19}$$

The corresponding non dimensional boundary conditions

$$u = -1$$
 at  $y = \pm \eta$ 

$$\frac{\partial^2 u}{\partial y^2} = 0 \quad \text{at} \quad y = \pm \eta$$

$$y = 0 \quad \text{at} \quad y = 0$$
(20)

Solving the equations subject to boundary conditions we

$$u = T_1 \cosh \alpha y + T_2 \cosh \beta y - \frac{dp / dx}{L^2}$$
(21)

$$u_p = T_3 \cosh \alpha y + T_4 \cosh \beta y + T_5 \tag{22}$$

$$v = v_p = -\frac{T_6 \sinh \alpha y}{\alpha} - \frac{T_7 \sinh \beta y}{\beta}$$
(23)

Knowing the velocity, the volume flow rate q in a wave frame of reference is given by

$$q = \int_{0}^{\eta} u dy = \frac{T_1 \sinh \alpha \eta}{\alpha} + \frac{T_2 \sin \beta \eta}{\beta} - \frac{(dp / dx)\eta}{M^2}$$
(24)

The pressure gradient is

$$\frac{dp}{dx} = \frac{L^2 \left( q + \frac{\tanh \alpha \eta}{\alpha \left( 1 - \frac{\alpha^2}{\beta^2} \right)} + \frac{\tanh \beta \eta}{\beta \left( 1 - \frac{\beta^2}{\alpha^2} \right)} \right)}{\frac{\tanh \alpha \eta}{\alpha \left( 1 - \frac{\alpha^2}{\beta^2} \right)} + \frac{\tanh \beta \eta}{\beta \left( 1 - \frac{\beta^2}{\alpha^2} \right)} - \eta} \tag{25}$$

where 
$$\alpha^2 = \frac{1 + \sqrt{1 - 4SL^2}}{2S}$$
,  $\beta^2 = \frac{1 - \sqrt{1 - 4SL^2}}{2S}$ ,  $L^2 = M^2 + \frac{1}{k_1}$ 



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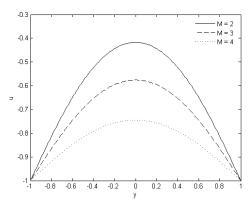
$$\begin{split} T_1 &= \left(\frac{dp/dx}{L^2} - 1\right) \frac{1}{\cosh \alpha \eta} \left(1 - \frac{\alpha^2}{\beta^2}\right), \\ T_2 &= \left(\frac{dp/dx}{L^2} - 1\right) \frac{1}{\cosh \beta \eta} \left(1 - \frac{\beta^2}{\alpha^2}\right), \\ T_3 &= \frac{T_2 S \tau \beta^4}{R \alpha_1} - \frac{T_2 \beta^2 \tau}{R \alpha_1} + T_2 \left(\frac{R \alpha_1}{\tau} + L^2\right), \\ T_4 &= \frac{T_1 S \tau \alpha^4}{R \alpha_1} - \frac{T_1 \alpha^2 \tau}{R \alpha_1} + T_1 \left(\frac{R \alpha_1}{\tau} + L^2\right), \\ T_5 &= \frac{(dp/dx)\tau}{R \alpha_1} - \left(\frac{R \alpha_1}{\tau} + L^2\right) \frac{(dp/dx)}{L^2} \cdot \frac{\tau}{R \alpha_1}, \\ T_6 &= \frac{\left(\frac{dp/dx}{L^2} - 1\right)\alpha \sinh \alpha \eta \left(2\pi\varepsilon \cos(2\pi x)\right)}{\cosh^2 \alpha \eta \left(1 - \frac{\alpha^2}{\beta^2}\right)} \end{split}$$

$$T_7 = \frac{\left(\frac{dp/dx}{L^2} - 1\right)\beta \sinh \beta \eta \left(2\pi\varepsilon \cos(2\pi x)\right)}{\cosh^2 \beta \eta \left(1 - \frac{\beta^2}{\alpha^2}\right)}$$

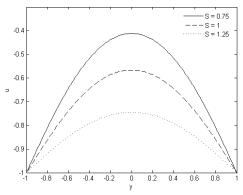
# 4. GRAPHICAL RESULTS AND DISCUSSIONS

This section provides the behavior of various parameters like the variations of coefficient of couple stress S, Hartmann number (M), permeability of the porous medium  $(k_1)$  involved in the expressions of velocity profile of the fluid (u), and the pressure gradient (dp/dx) are tested.

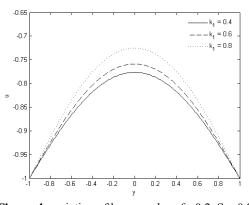
The behaviour of Hartmann number on velocity profile is shows in Figure-2. Figure-2 depicts that the Hartmann number (M) increases as velocity profile of the fluid (u) decreases. The behavior of couple stress parameter on velocity profile is shows in Figure-3. It depicts that the couple stress parameter (S) increases as velocity profile of the fluid (u) decreases. The behavior of permeability parameter of porous medium  $k_1$  on velocity profile u is shows in Figure-4. It depicts that the pressure gradient  $k_1$  increases as velocity profile of the fluid (u) increases.



**Figure-2.** Variation of *M* on *u* when  $\varepsilon$  =0.2, S=0.75, dp/dx=1, k<sub>1</sub>= 0.5.



**Figure-3.** variation of *S* on *u* when  $\varepsilon = 0.2$ , dp/dx = 1, M=2, k1=0.5.



**Figure-4.** variation of  $k_1$  on u when  $\varepsilon = 0.2$ , S = 0.75, dp/dx = 1, M = 2.

The behavior of couple stress parameter is shows in Figure-5 on dp/dx. Figure-5 shows that couple stress parameter (S) increases as pressure gradient (dp/dx) decreases. The behavior of Hartmann number M on pressure gradient is shown in Figure-6. It depicts that the Hartmann number increases as pressure gradient increases. Figure-7 depicts that the permeability of the porous

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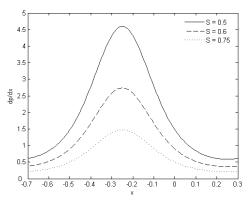
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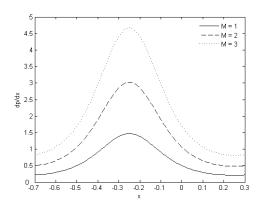


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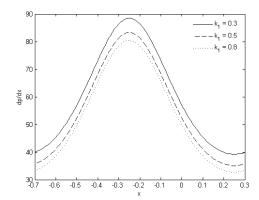
medium  $k_1$  decreases as pressure gradient (dp/dx) increases.



**Figure-5.** variation of S on dp/dx when  $\varepsilon = 0.1$ , M=1,  $k_1 = 0.5$ .



**Figure-6.** Variation of M on dp/dx when  $\varepsilon = 0.1$ , S=0.75,  $k_1 = 0.5$ .



**Figure-7.** variation of  $k_1$  on dp/dx when  $\varepsilon = 0.1$ , S = 0.75, M = 1, 2, 3.

# 5. CONCLUSIONS

The influence of couple stress fluid on the MHD peristaltic flow through suspended particles in two dimensional flexible channels through a porous medium has been analyzed. The problem has been solved under

long wave length and low Reynolds number approximation. Analytical solution have been developed for velocity profile and pressure gradient. The results calculated for velocity profile and pressure gradient. The features of flow characteristics are analysed by plotting graph and discussed in detail. The amin findings are summarized as follows.

It is observed that u decreases with increase in Hartmann number M and dust characterizing parameter S. Velocity profile increases as the permeability of the porous medium increases.

The pressure gradient (dp/dx) has an opposite results compared with u for M. pressure gradient decreases as permeability parameter increases.

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